



Softell grade for interiors: CAE validation for a Jaguar Land Rover project using *Digimat*

M.Nutini - Basell Poliolefine Italia, a LyondellBasell Company

M.Blagdon - Jaguar Land Rover

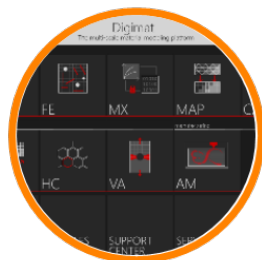
H.Skhiri - e_Xstream Engineering

Material meets Engineering Conference 2019

e-Xstream Engineering



e-Xstream



Digimat

The material & process modeling platform



MaterialCenter

Material Lifecycle Management Platform



MSC Software

Software for Virtual Validation & Optimization of Engineering Designs

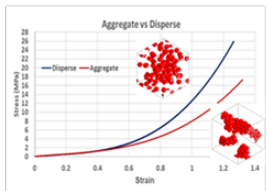


Hexagon

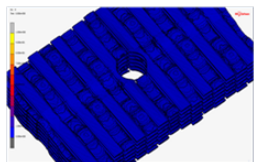
Digital Solutions Smartly Connecting the Physical & Digital Worlds

10x MATERIALS SOLUTION

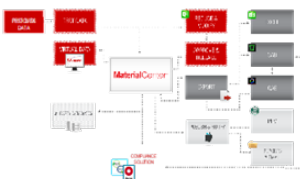
1 Virtual Material Development



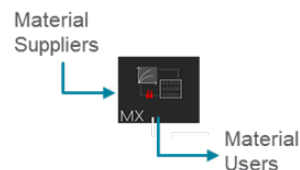
2 Virtual Material Testing



3 Materials Lifecycle Management



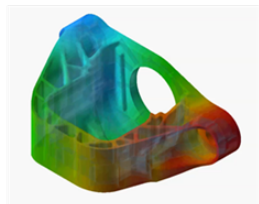
4 Material eXchange



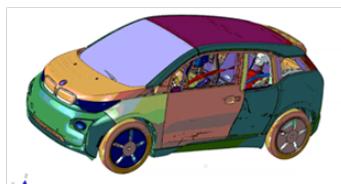
5 Compliance & Sustainability

Material	Material Type	Material Grade	Material Supplier	Material Location	Material Status
Aluminum 6061-T6	Aluminum	6061-T6	Aluminum Supplier	Aluminum Location	Aluminum Status
Steel A36	Steel	A36	Steel Supplier	Steel Location	Steel Status
Carbon Fiber	Carbon Fiber	Carbon Fiber	Carbon Fiber Supplier	Carbon Fiber Location	Carbon Fiber Status

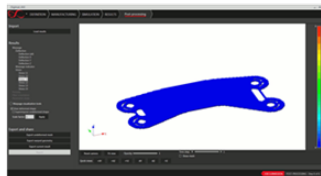
6 Effect of Processing



7 Accurate Material Modelling



8 (Additive) Manufacturing



9 Material Intelligence(AI)

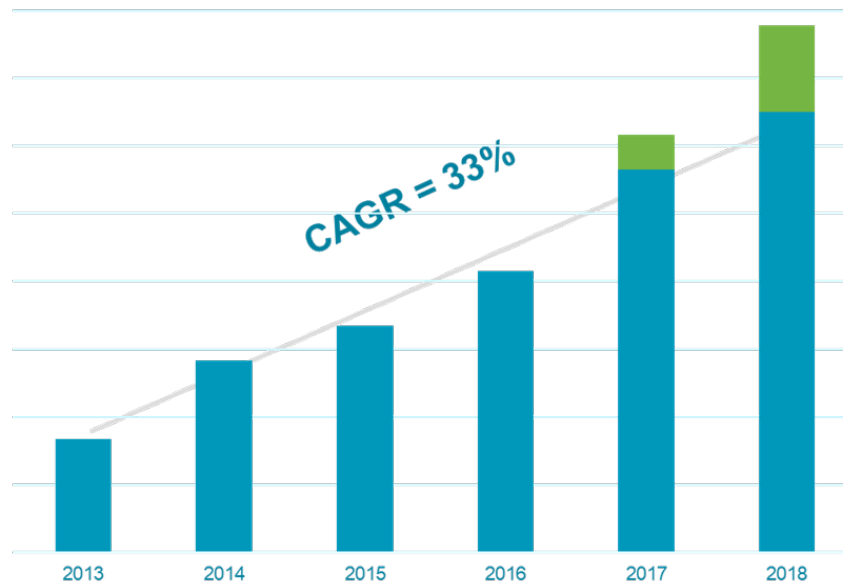
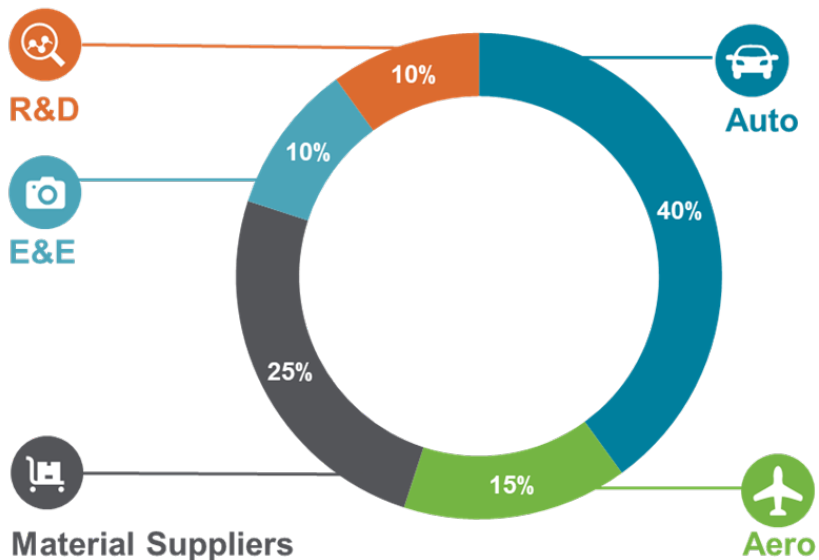


10 Digital Continuity & (Material)Twin



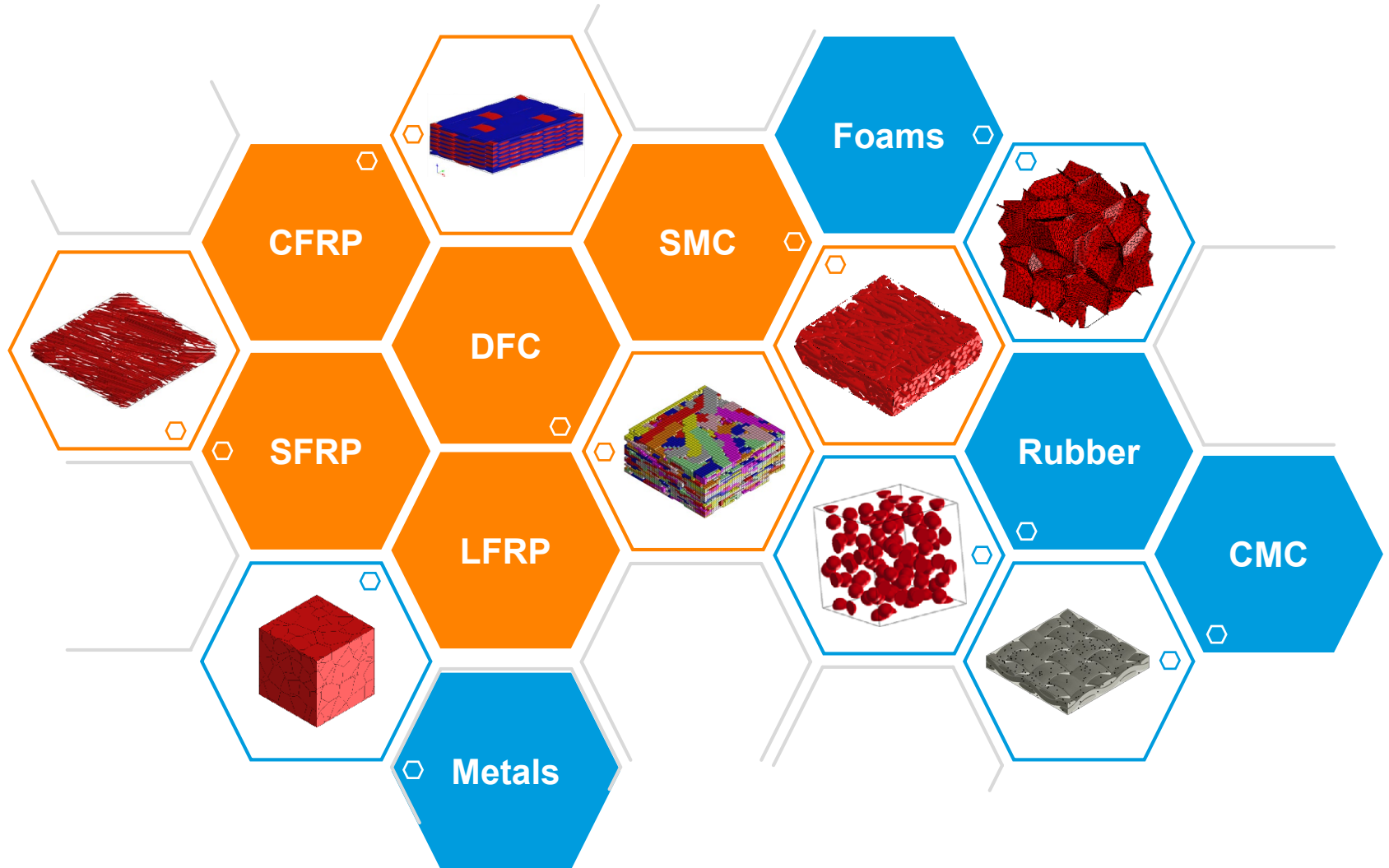
e-Xstream : 15 Years of Double Digit Growth!

500+ Customers, 3x Revenues growth in the last 5 years



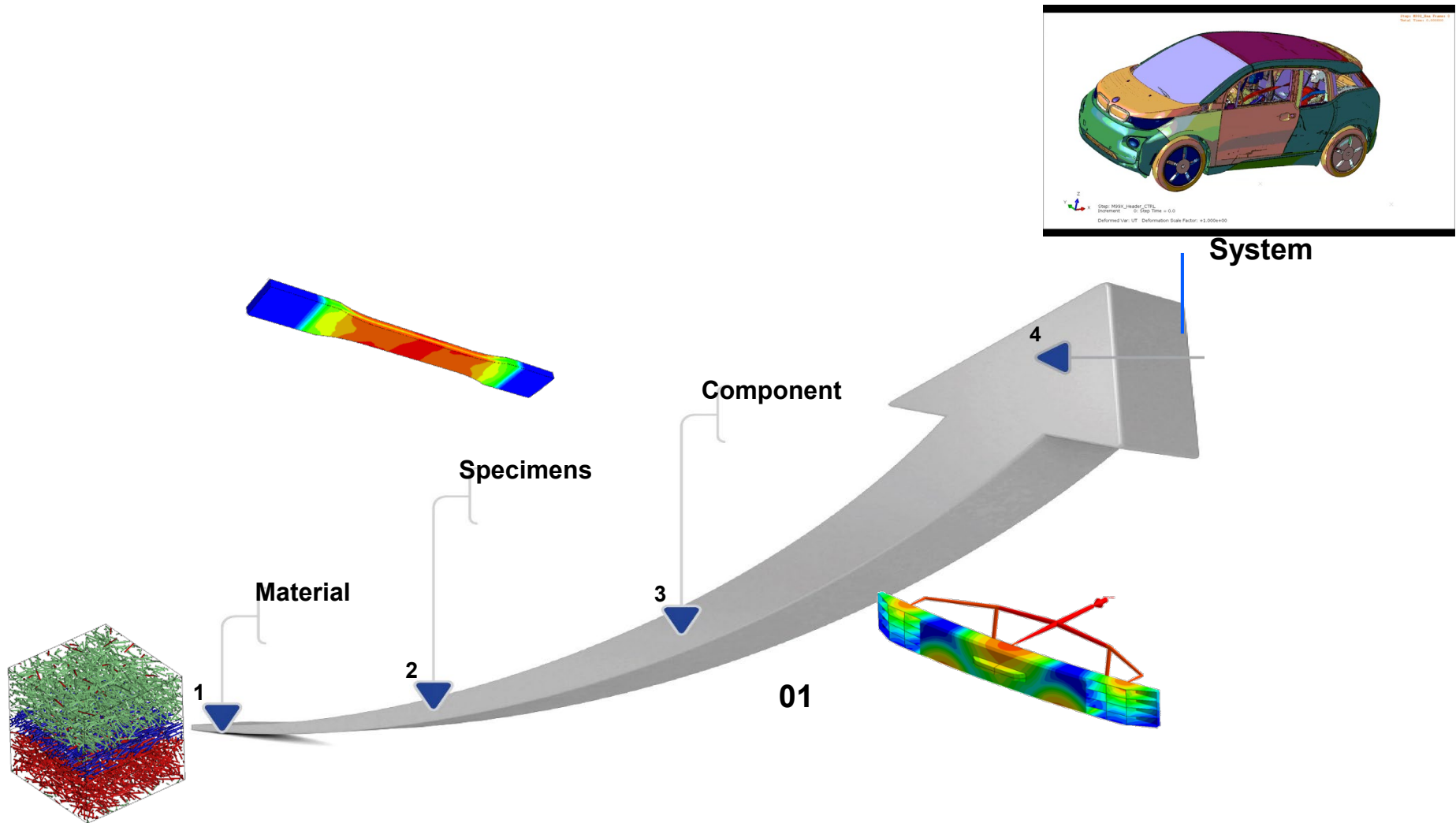
e-Xstream : Accurate, Robust, Fast & Easy Modeling of Material

Accelerated Investments in Addition Material Systems...



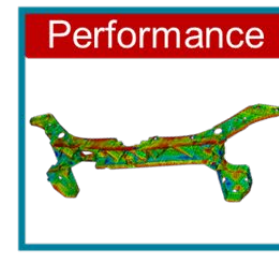
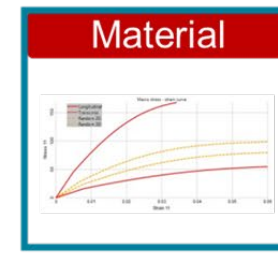
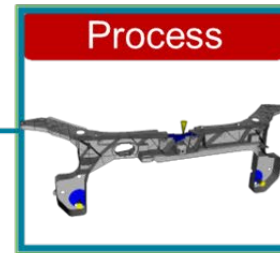
e-Xstream : Hierarchical Verification & Validation

From the material system to the full system



e-Xstream : Material Simulation to Reach Industry Requirements

Bridging the gap between disciplines & scales for faster/cheaper part development



- Select the right material for the right application
- Technical support for design, process optimization and CAE validation
- Shorten development time & reduce cost

Advanced Material Database & Simulation Workflow

Softell material- Goes to amazing extremes so tough yet so soft

■ Innovative Material in a wide range of automotive & non-automotive applications.

- High quality product performances
- Soft Touch
- Reduced system complexity
- Lower system cost
- Support of green objectives



Source: LyondellBasell

Why *Softell* compounds?

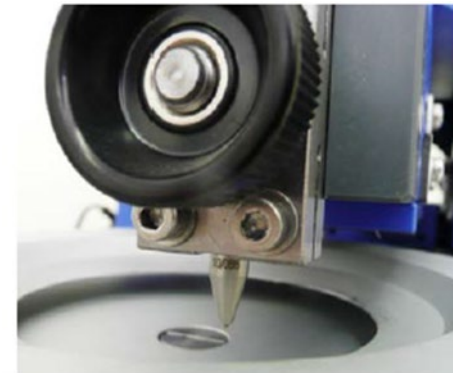
■ Tough, yet so soft!

- High quality finished part surfaces with soft touch and matt surface without painting
- Excellent scratch resistance and surface robustness
- Ductility at low temperature
- Good noise dampening properties
- Support “green objectives“ PP component concept allowing easy recycling



Soft Touch

Source: LyondellBasell

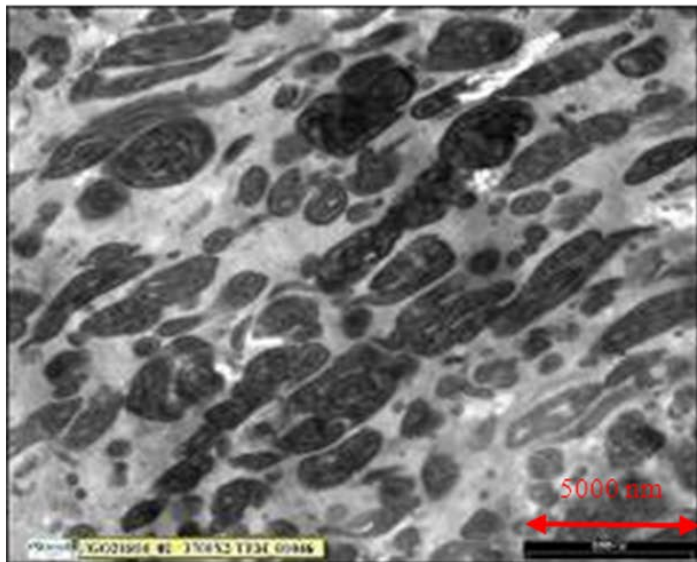


Scratch
Resistance

Source: LyondellBasell

What is *Softell* material?

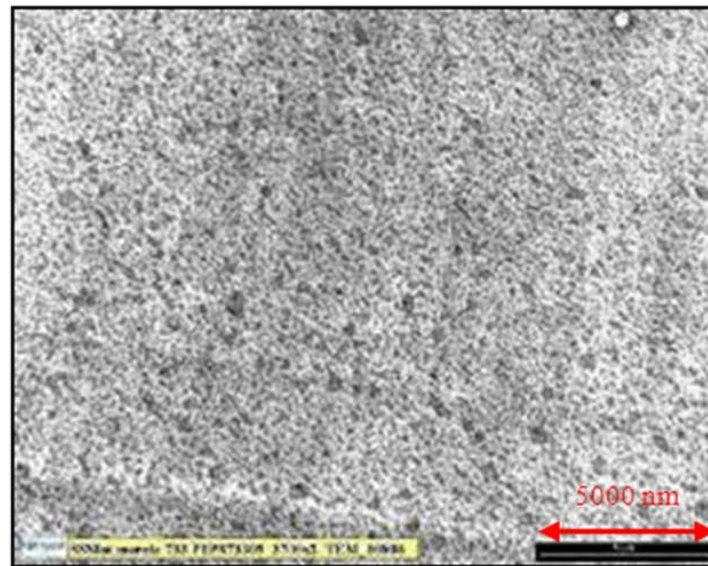
Physical blend of PP & Rubber



Source: LyondellBasell

Compounding process

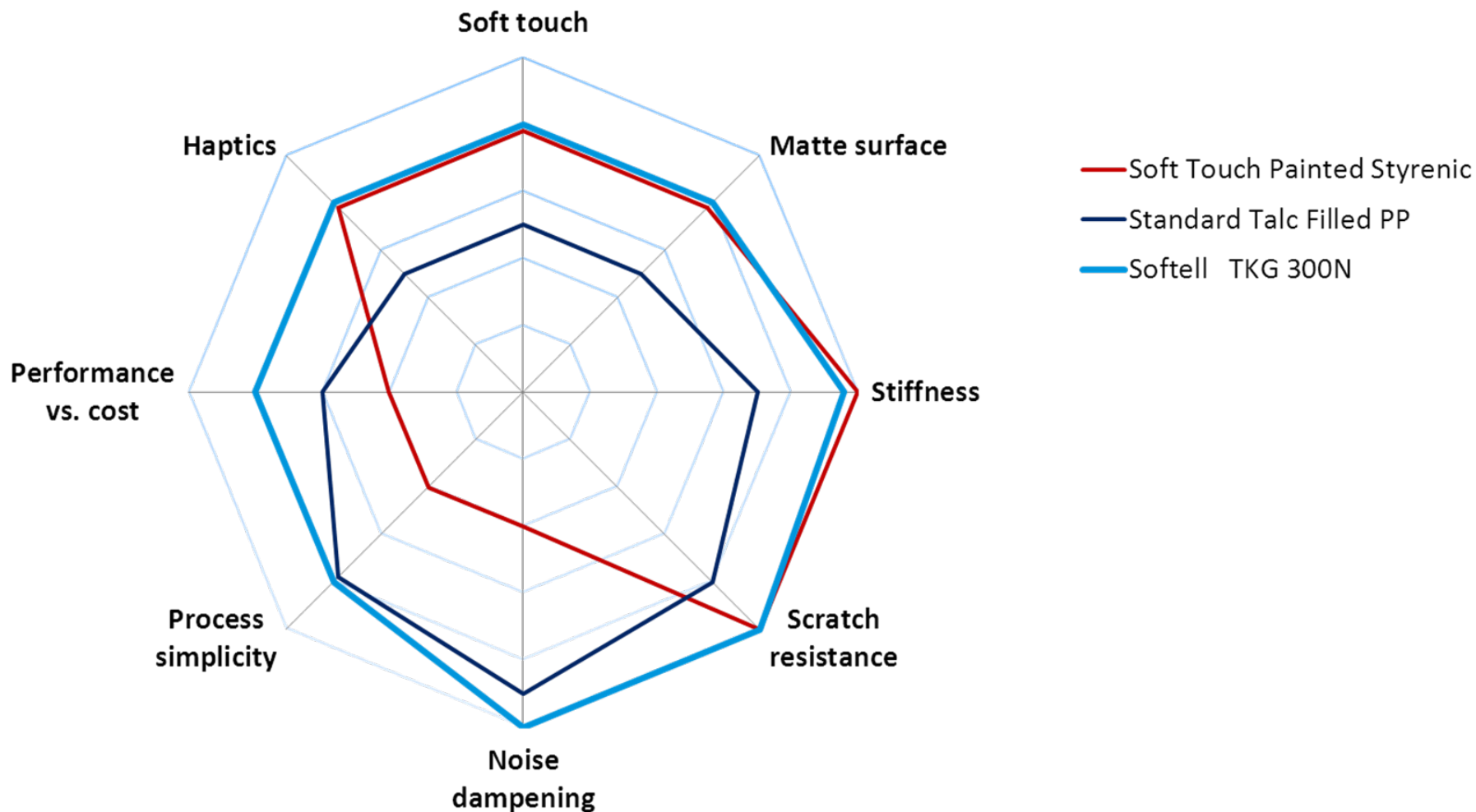
Softell by *Catalloy* process



Source: LyondellBasell

Catalloy polymerization process

Customer value of *Softell* resin blend





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Advancing Possible

LyondellBasell AND Jaguar Land Rover

Metallic Materials at Jaguar Land Rover

A combination of LyondellBasell Bumper materials in dark techno silver and light silver for the Range Rover Evoque



Source: Jaguar Land Rover

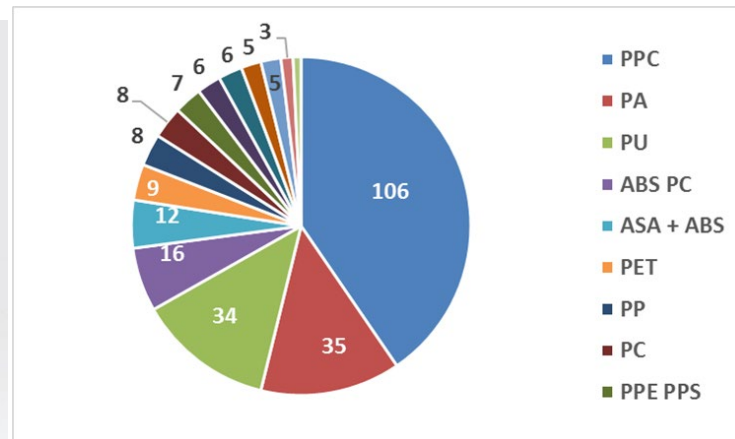
Future New Application Areas for Electric Vehicles



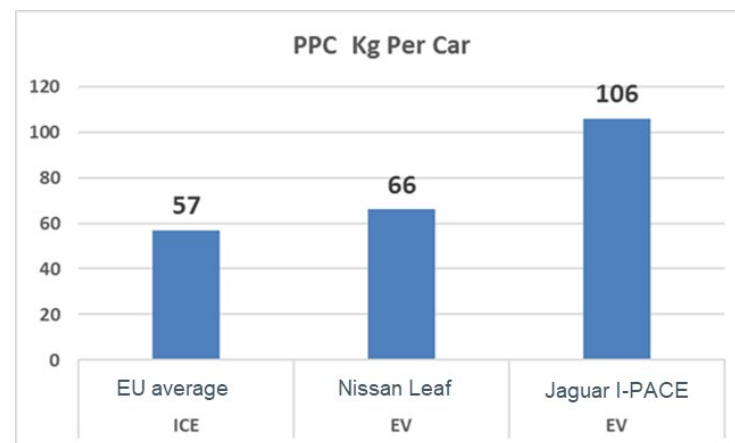
Source: Jaguar Land Rover

Jaguar I-PACE Bonnet Scoop

- The Jaguar I-PACE is using 106 Kgs of PP Compounds



Source: A2MAC1



Source: A2MAC1

Softell material at Jaguar Land Rover



Source: Jaguar Land Rover



Source: Jaguar Land Rover

Softell TKG 300N now used for many interior applications to replace PC/ABS for glove box doors and seat backs

Example: Jaguar XE



Source: Jaguar Land Rover



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Advancing Possible

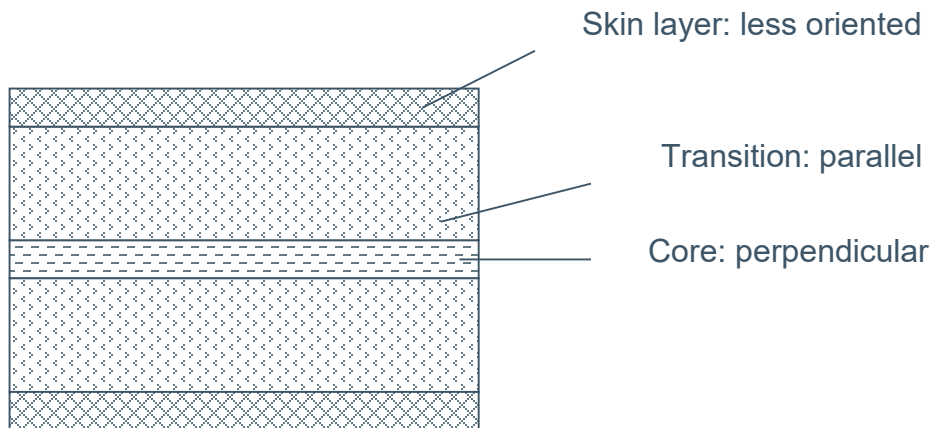
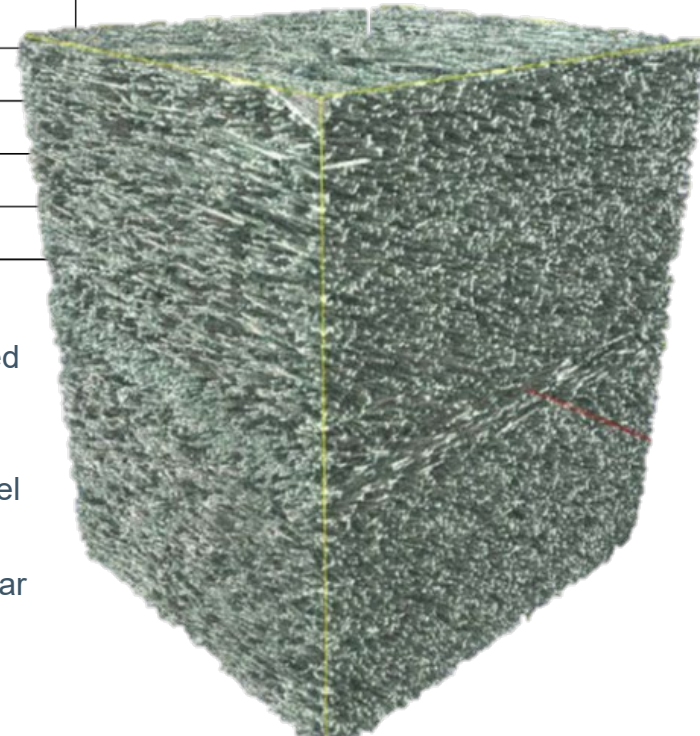
LyondellBasell AND e_Xstream

Process induced Anisotropy

Typical ratio of longitudinal vs. transverse properties of PP-based materials measured on an injection molded 3 mm thick plaque:

Material type	Transv/Long Moduli ratio	Transv/Long Max stress ratio
40% SGF-PP homopolymer	0.5	0.56
30% SGF-PP homopolymer	0.63	0.67
10% SGF-PP homopolymer	0.86	0.82
25% SGF-PP Soft PP	0.57	0.68
Impact modified PP/Talc	0.81	0.83
Unfilled PP copolymer	0.93	0.93

- Anisotropy is affected by:
- Filler/ reinforcement type
 - Filler/ reinforcement amount
 - Process parameters



Here: flow lines perpendicular to the sheet

Source: LyondellBasell

Source: LyondellBasell

Process induced Anisotropy

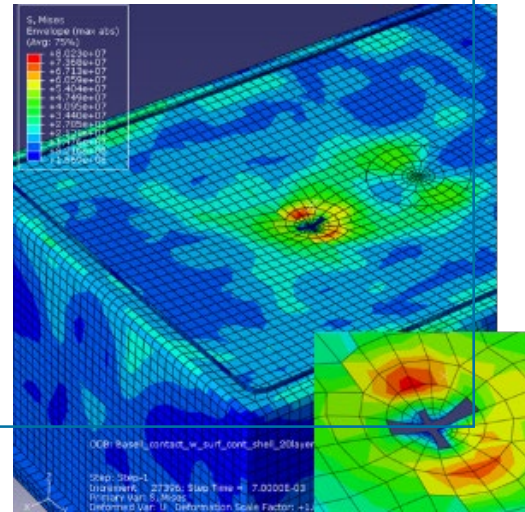
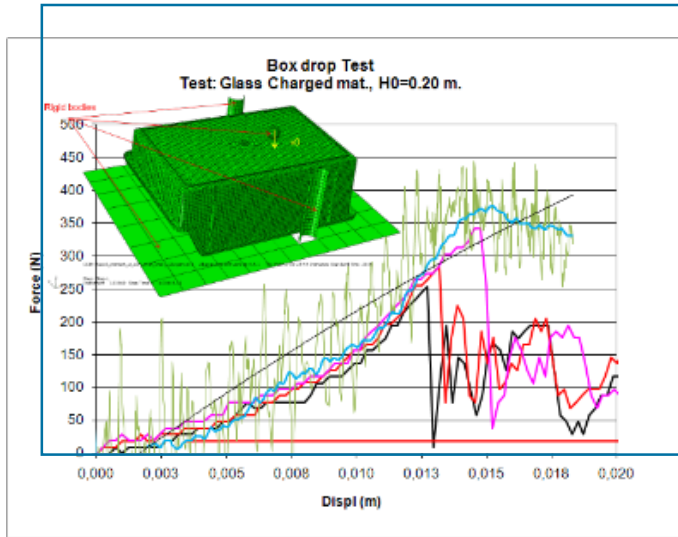
Two main approaches currently available with F.E. analysis

	Micro-mechanical modeling (e.g. e-Xstream Digimat®)	Simplified anisotropic (internal LyondellBasell development)
Material Law	Dedicated, based on Mean field homogenization theories (Digimat by e-Xstream, coupled with most FE codes)	Orthotropic / anisotropic (e.g. Abaqus orthotropic, Ls-dyna MAT_157)
Input from Process Simulation (e.g. Moldflow)	Fiber orientation	Fiber Orientation/ Flow direction
Experimental data	Tensile test in two or more directions	Tensile test in two or more directions

The choice of the approach depends on the specific problem to be studied and on the “boundaries,” such as resources, requested accuracy and timing.

Digimat has all the features needed for this project and was therefore chosen.

LyondellBasell and *Digimat*: brief history (1 of 2)



2009: *Digimat* test by e_Xstream on the «Nutini» box (Basell Validation tool)

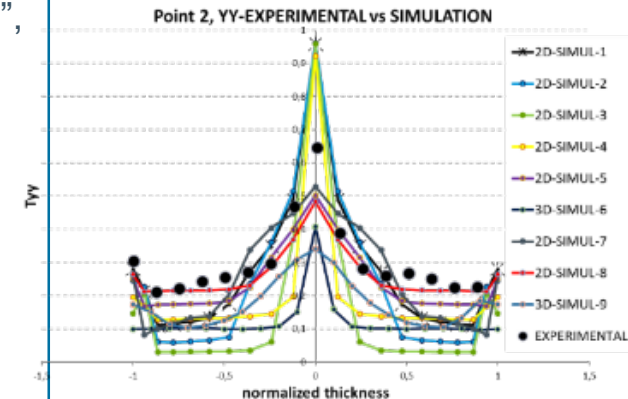
Source: LyondellBasell

C.Garcia, M.Nutini, “Fiber Orientation Prediction for Reliable Simulations of Glass-reinforced, Polypropylene-based Components Using DIGIMAT”, Digimat Users Meeting, Luxembourg, October 2010

M.Nutini, “An assessment of fiber orientation in GF-PP compounds by assembling the information from testing, mold filling simulation and Digimat-MF through optimization methods”, Digimat Users Meeting, Munich, October 2011

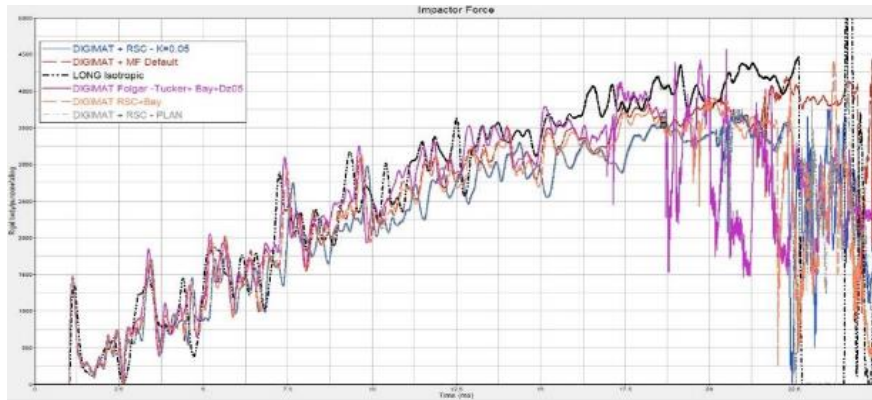
C.Ferrari, C.Garcia, M.Nutini, “Assessment of Fiber Orientation in Injection-Molded SGF-PP items”, Connect! Moldflow Users Meeting 2011, Frankfurt, May 2012

2010/2012: Basell validation studies



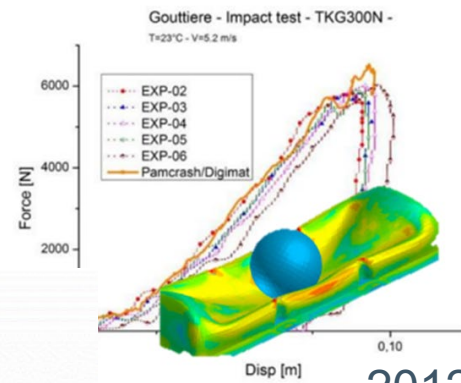
Source: LyondellBasell

LyondellBasell and *Digmat*: brief history (2 of 2)



Source: LyondellBasell

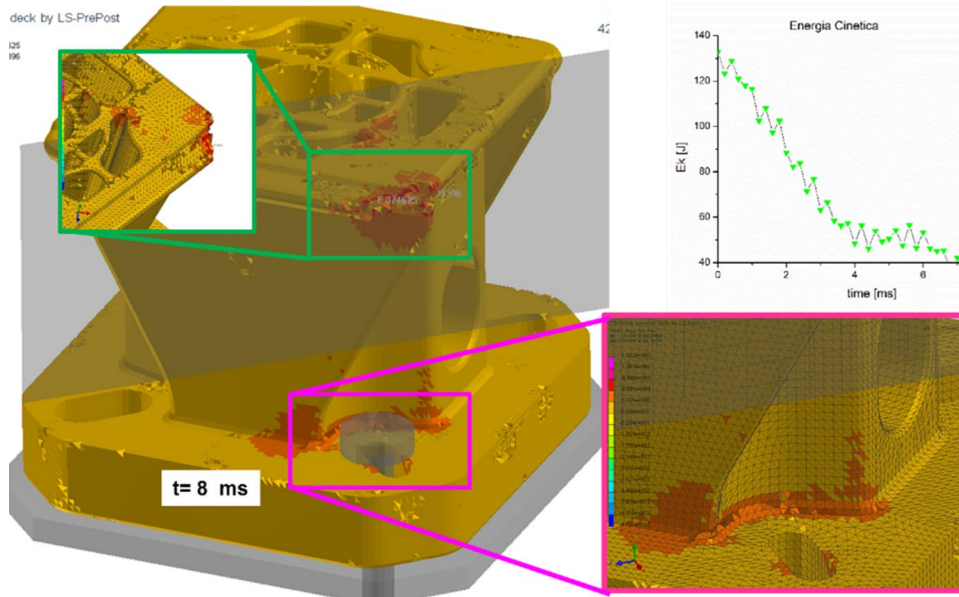
2012-2014: Support in the project of a lower bumper stiffener (Activity with Opel, Materials Meet Engineering, 2012)



Source: LyondellBasell



2012: Support in the project of a door panel (Activity with Renault, Materials Meet Engineering, 2012)



Source: LyondellBasell

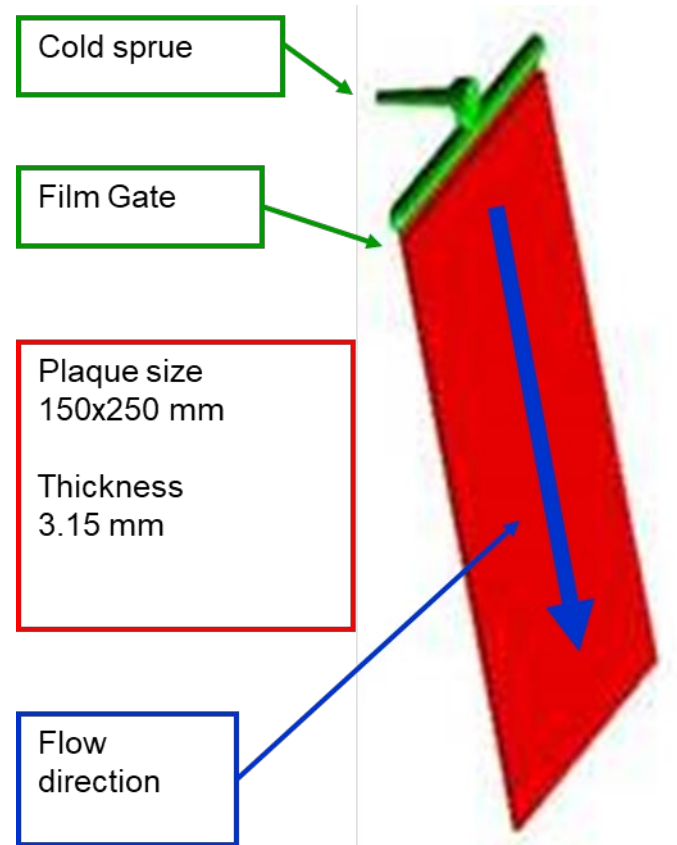
2018: Design of a part for building and construction industry (Activity with Polytech, Digmat Tech. Day, 2018)



Modelling *Softell* material for Impact Simulation

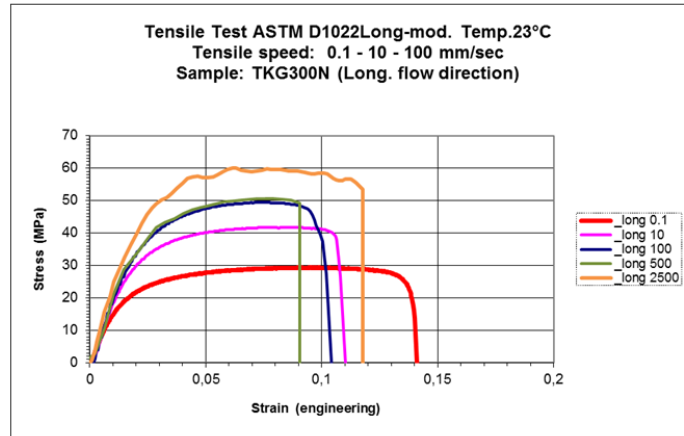
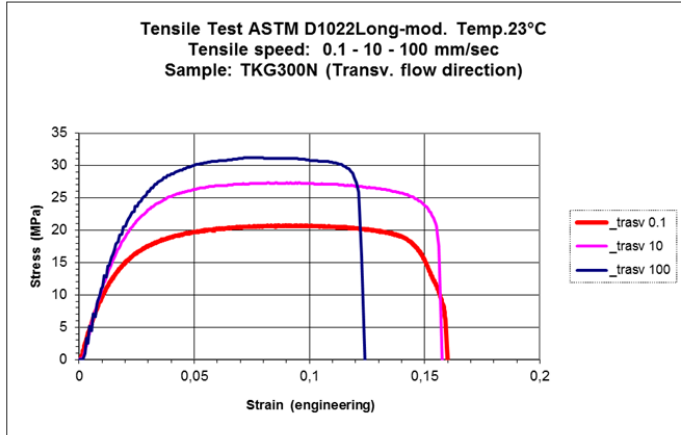
Softell material: Experimental data

- **LyondellBasell testing method for GF-PP: mechanical properties are better measured on specimens cut from injection-molded plaques.**
 - The material orientation in the plaque is similar to the one existing in the real components, while in injection molded specimens the orientation is emphasize
 - It is possible to cut specimens along any desired direction with respect to injection flow. Here specimens cut at 0° and 90° with respect to the flow direction in the mold have been used

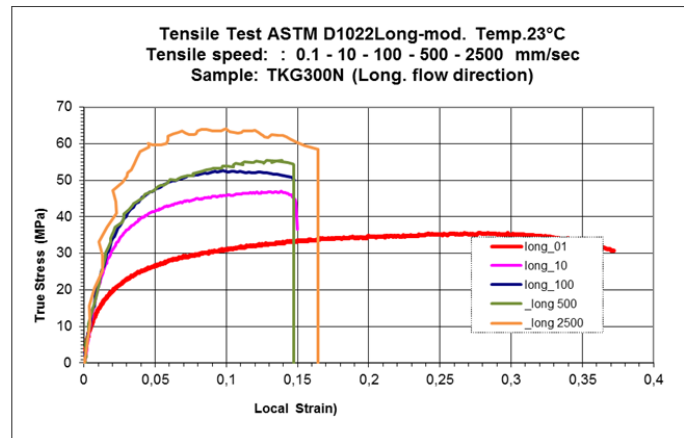
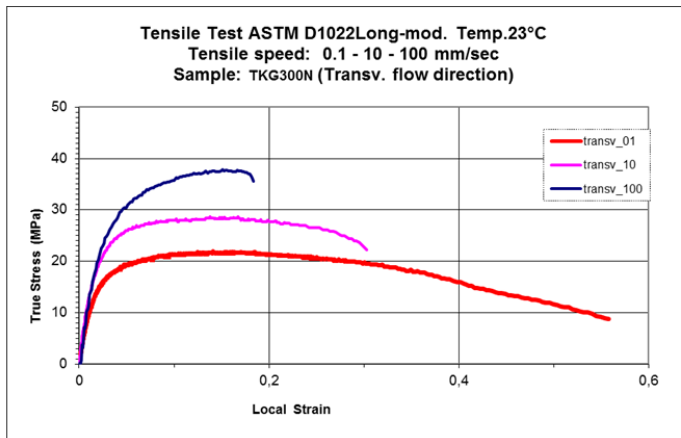


Source: LyondellBasell

Softell material: Experimental data



Engineering curves



Curves from Local strain measurement

Source: LyondellBasell

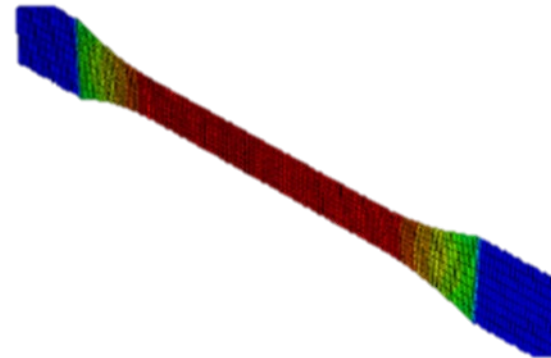
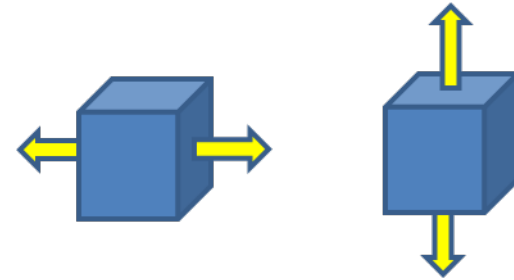
Building up a *Digimat* material card

■ Determination of Elastic Parameters

- Based on average fiber orientation
- Pure uniaxial loading
- Determination of elastic parameters
- First Guess of Plasticity-related parameters

■ Tensile test validation: tuning of plasticity parameters

- Based on distributed fiber orientation
- Not-pure uniaxial loading (striction and volume change)
- Tuning of Plasticity-related parameters
- Introduction and validation of a failure criterion



Source: LyondellBasell

Exponential and linear law,
 $R(p) = kp + R_1[1 - \exp(-mp)]$.

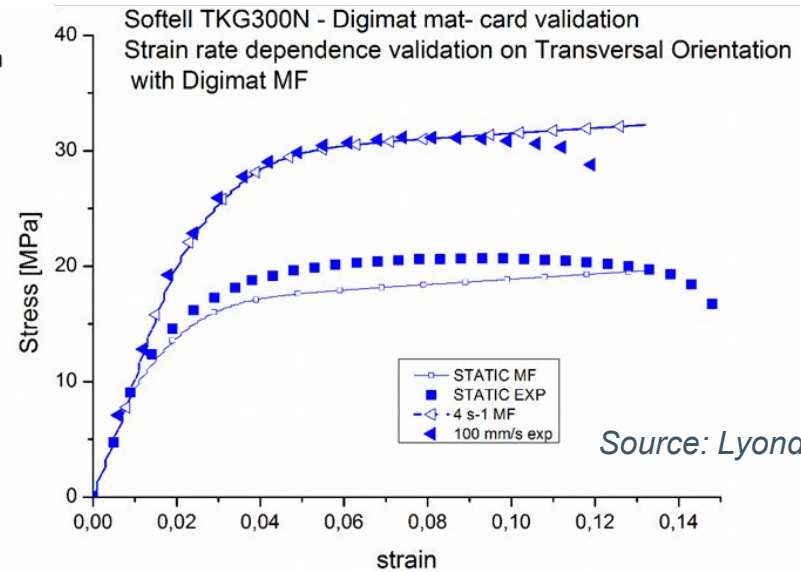
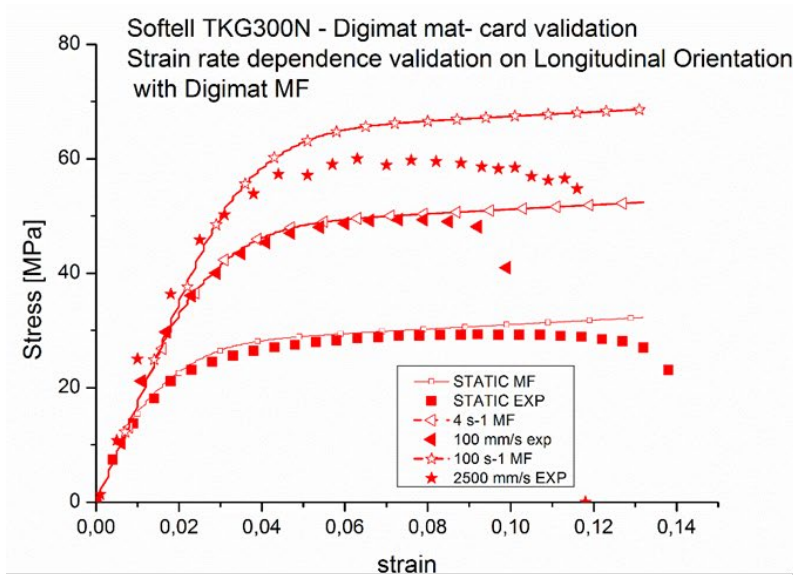
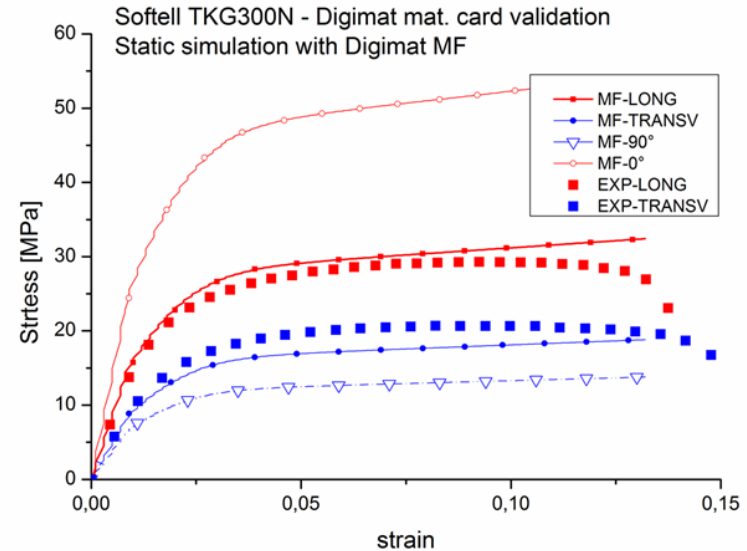
Material card preparation and validation on the tensile test

■ STATIC

- Identification of the parameters for static behavior modelling, including extreme /untested orientations, via *Digmat* MF and then FEM simulation

■ DYNAMIC

- Identification of the parameters for dynamic behavior modelling, via *Digmat* MF



Source: LyondellBasell

Introducing a failure criterion

■ Preferred choice: Tsai-Wu interactive criterion

- Anisotropic
- Compression/tension sensitive
- Interactive
- Strain/rate dependent

Tsai_Wu 3D, stress-based

Failure indicator:

$$f_A \text{ is such that } \mathcal{F}_A(\boldsymbol{\sigma}/f) = 1, \text{ with}$$

$$\mathcal{F}_A(\boldsymbol{\sigma}) = \frac{\sigma_{11}^2}{X_t X_c} + \frac{\sigma_{22}^2 + \sigma_{33}^2}{Y_t Y_c} + \frac{\sigma_{12}^2 + \sigma_{13}^2}{S^2} + \frac{4\sigma_{23}^2}{Y_t Y_c} - \frac{\sigma_{11}\sigma_{22} + \sigma_{11}\sigma_{33}}{2X_t X_c} - \frac{2\sigma_{22}\sigma_{33}}{Y_t Y_c} + \left(\frac{1}{X_t} - \frac{1}{X_c}\right)\sigma_{11} + \left(\frac{1}{Y_t} - \frac{1}{Y_c}\right)(\sigma_{22} + \sigma_{33})$$

Tsai_Wu 3D, strain-based

Failure indicator:

$$f_A \text{ is such that } \mathcal{F}_A(\boldsymbol{\epsilon}/f) = 1, \text{ with}$$

$$\mathcal{F}_A(\boldsymbol{\epsilon}) = \frac{\epsilon_{11}^2}{X_t X_c} + \frac{\epsilon_{22}^2 + \epsilon_{33}^2}{Y_t Y_c} + \frac{(2\epsilon_{12})^2 + (2\epsilon_{13})^2}{S^2} + \frac{(2\epsilon_{23})^2}{Y_t Y_c} - \frac{\epsilon_{11}\epsilon_{22} + \epsilon_{11}\epsilon_{33}}{2X_t X_c} - \frac{2\epsilon_{22}\epsilon_{33}}{Y_t Y_c} + \left(\frac{1}{X_t} - \frac{1}{X_c}\right)\epsilon_{11} + \left(\frac{1}{Y_t} - \frac{1}{Y_c}\right)(\epsilon_{22} + \epsilon_{33})$$

when the normal to the plane of isotropy corresponds to axis 1,

$$\Lambda(\dot{\epsilon}) = \Lambda_0 \left[1 + \left(\log \frac{\dot{\epsilon}}{\dot{\epsilon}_{\text{ref}}} \right)^{1/p} \right],$$

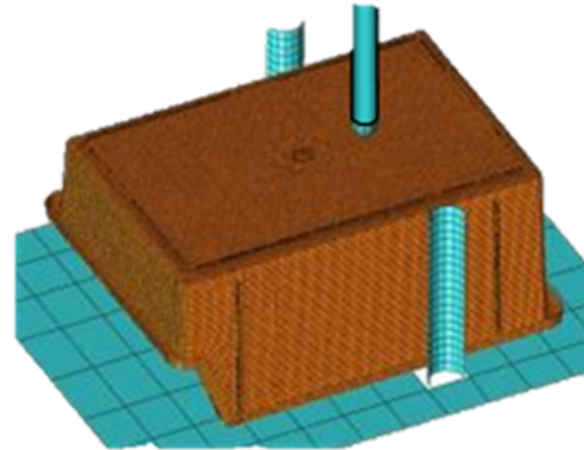
The material elongations at break are the parameters to be tuned and validated

1st Validation: LyondellBasell test case

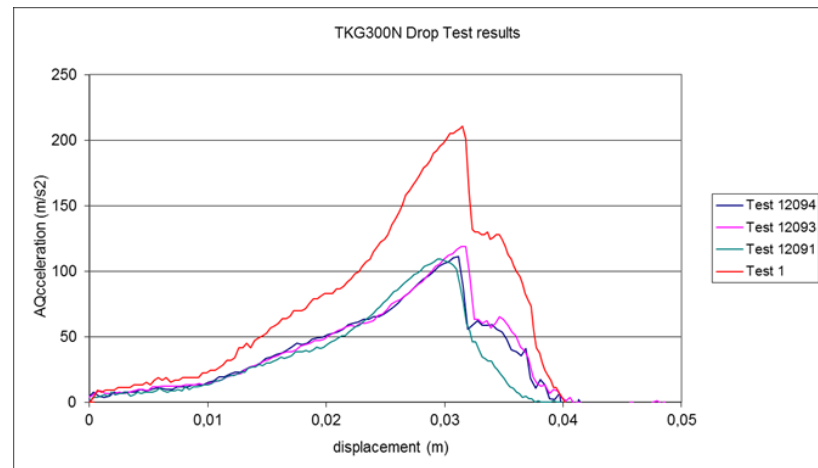
1st validation: LyondellBasell test case

■ “Dart Test: Test on LyondellBasell Box

- Drop test
- Several parameters used.
- “Test1” (in the graph) is the test chosen
- Impactor Mass: 5.186 Kg
- Impactor diameter 20 mm
- Falling height: 0.6 m
- Force vs. displacement recorded



Source: LyondellBasell

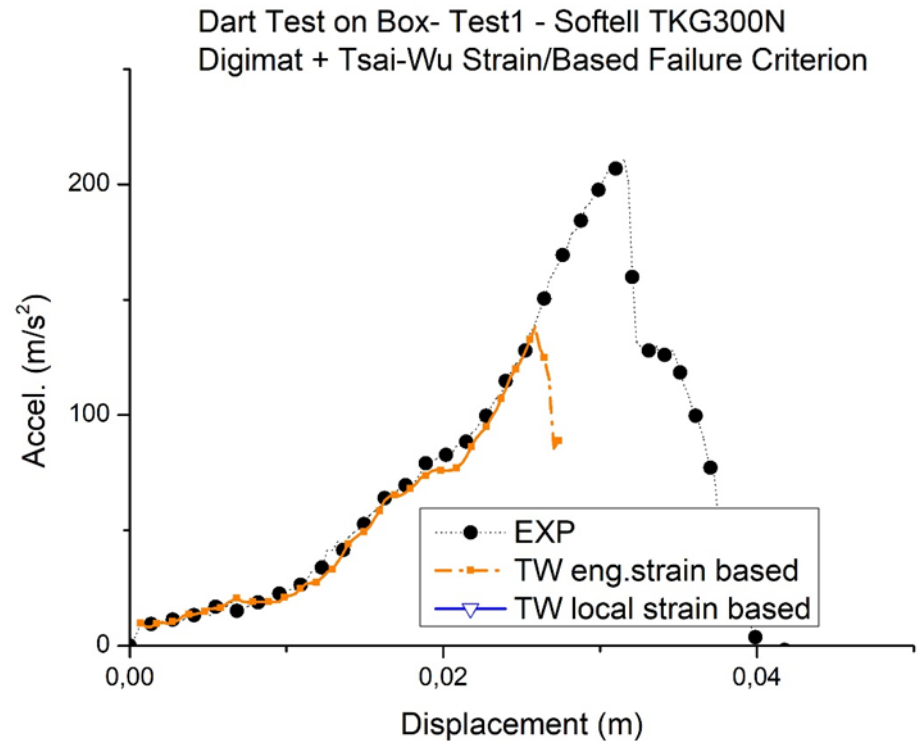


Source: LyondellBasell

1st validation: LyondellBasell test case

■ Results

- Good reproduction of the Force vs. Displacement: elasticity, plasticity and viscoplasticity parameters in the Material Card are OK
- Premature rupture onset with the Tsai-Wu strain-based failure criterion built on the engineering strains
- Fracture propagation strongly influenced by the mesh; unrealistic fracture surfaces are obtained

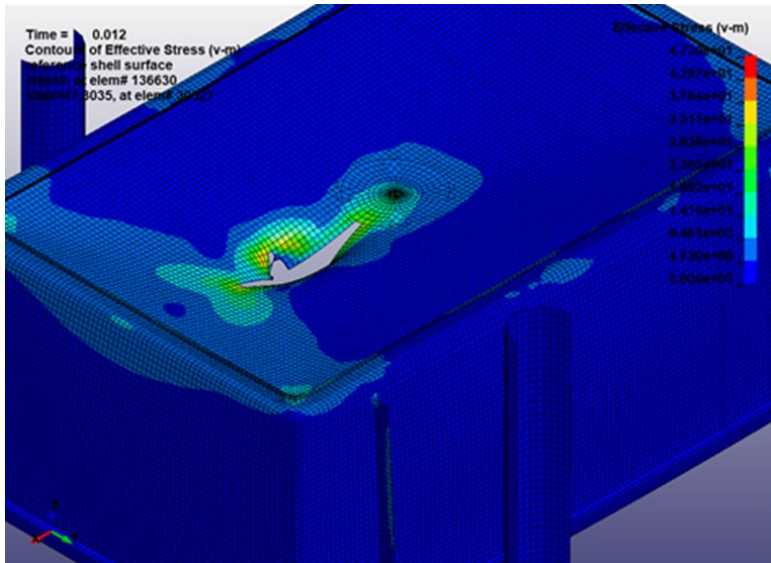


Source: LyondellBasell

1st validation: LyondellBasell test case

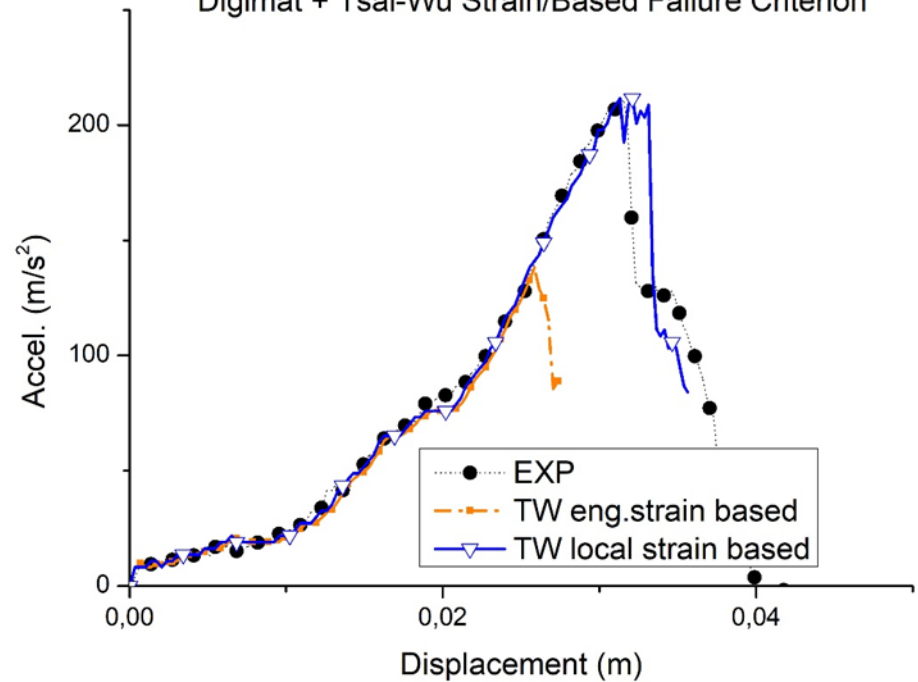
■ Modification: Tsai Wu based on LOCAL strain

- The introduction of local strains definitely improves the prediction of the onset of failure
- Still unrealistic fracture surfaces are obtained



Source: LyondellBasell

Dart Test on Box- Test1 - Softell TKG300N
Digimat + Tsai-Wu Strain/Based Failure Criterion

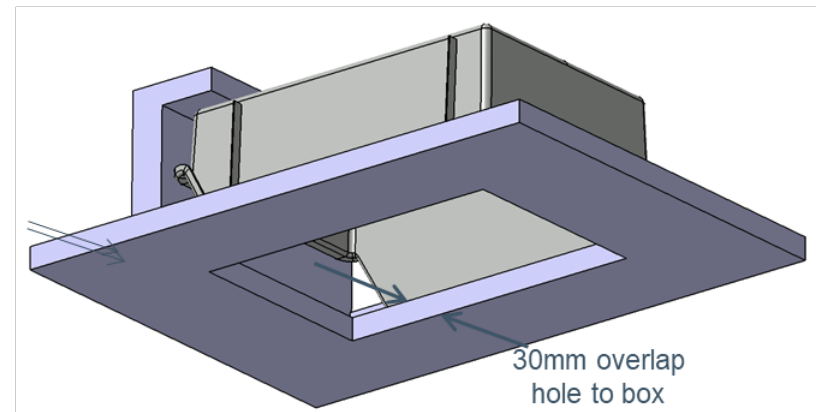
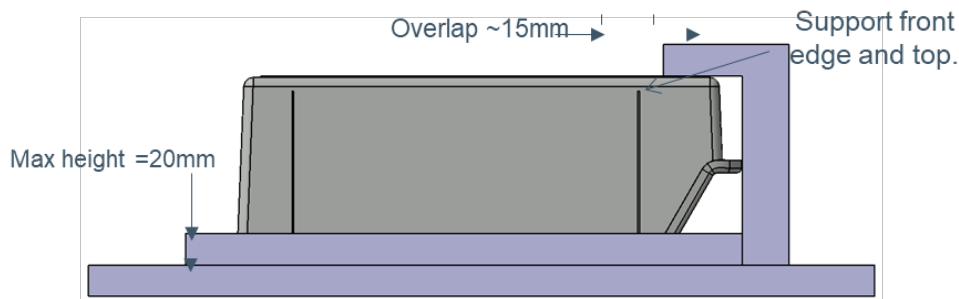
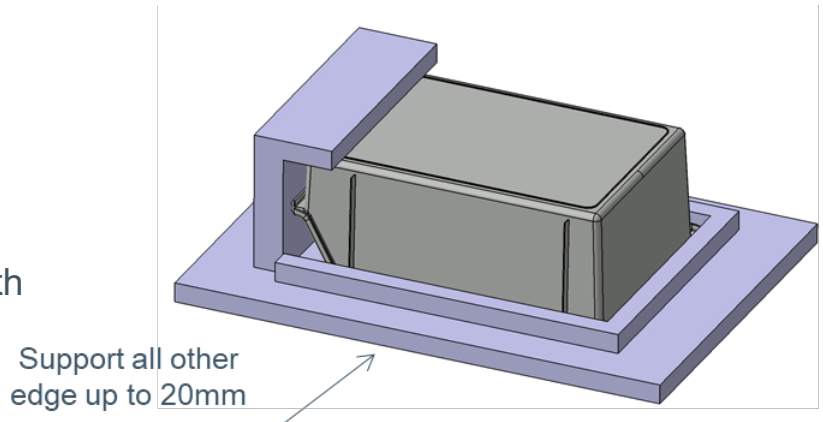


Source: LyondellBasell

2nd Validation: Jaguar Land Rover test case

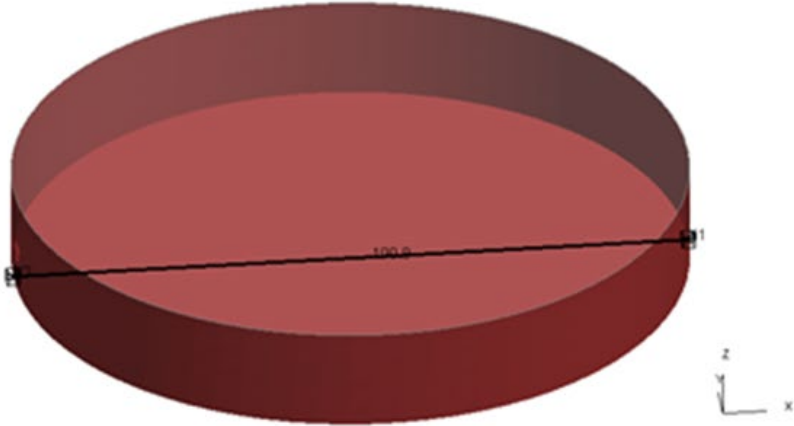
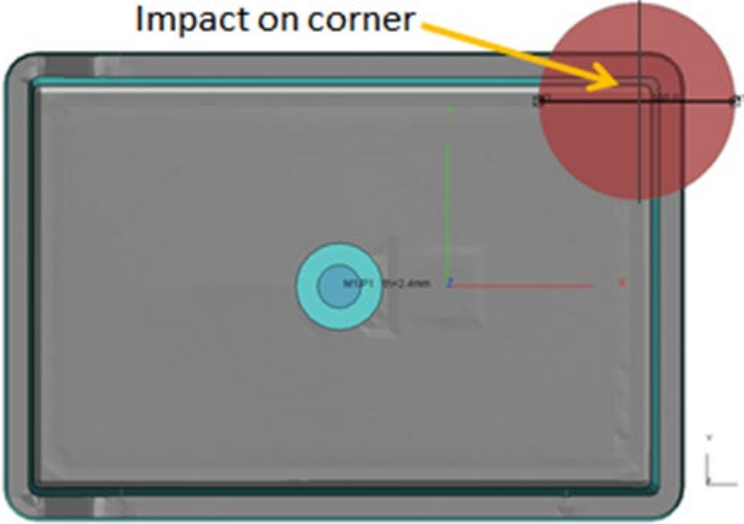
Jaguar Land Rover test case: layout

- During some of the impacts the front edge of the box will have a tendency to lift. To reduce variability of the results all edge will be constrained in the following configuration.
- If possible the rig will contain a hole underneath to capture deformation pattern will optical measurement cameras.



Source: Jaguar Land Rover

Jaguar Land Rover test case: layout

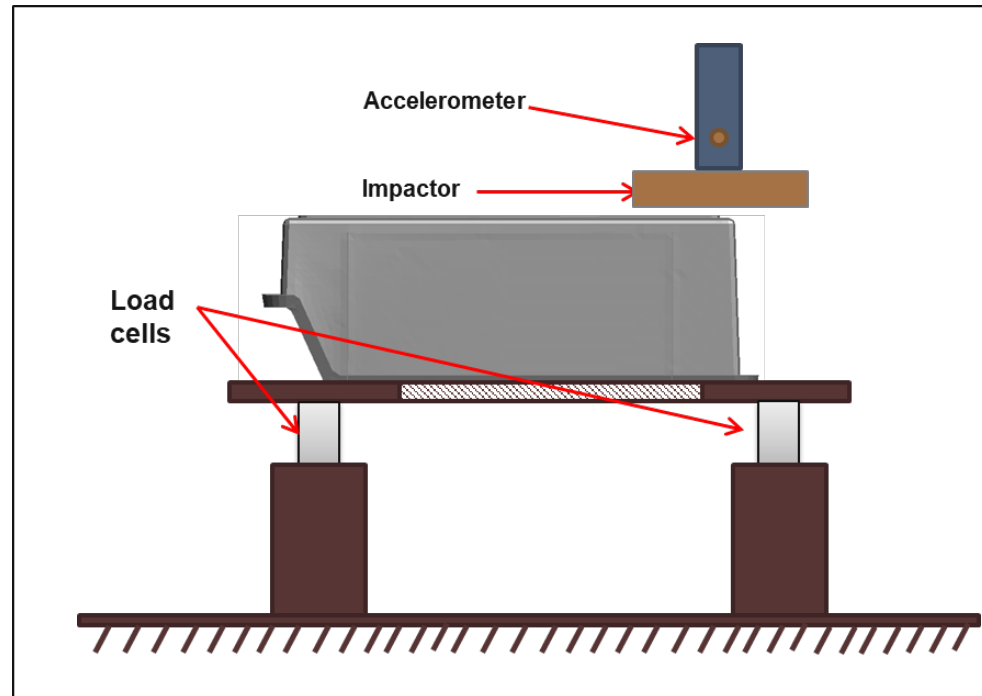
<u>Impactor Type</u>	<u>Location</u>
Flat Disk Impact and Quasi Static Test – Box Corner Crush	
<p data-bbox="311 454 799 496">~100mm flat disk impactor</p> 	<p data-bbox="1141 482 1431 525">Impact on corner</p> 

Source: Jaguar Land Rover

Jaguar Land Rover test case: layout

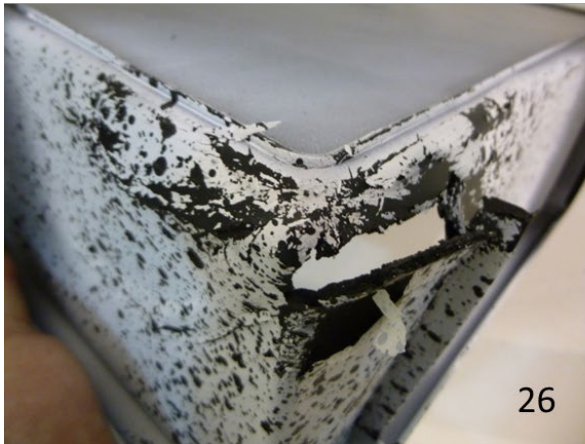
■ Drop test

- Drop rig total mass = ~10kg
- Drop Energy = ~150J
- Impact Velocity = 5.5m/s
- Equivalent Drop Height = 1500mm
- Impact Acceleration Recorded
- Loadcell under fixture or on impactor
- Displacement laser
- Optical Measurement cameras



Source: Jaguar Land Rover

Jaguar Land Rover test case: results



Source: Jaguar Land Rover

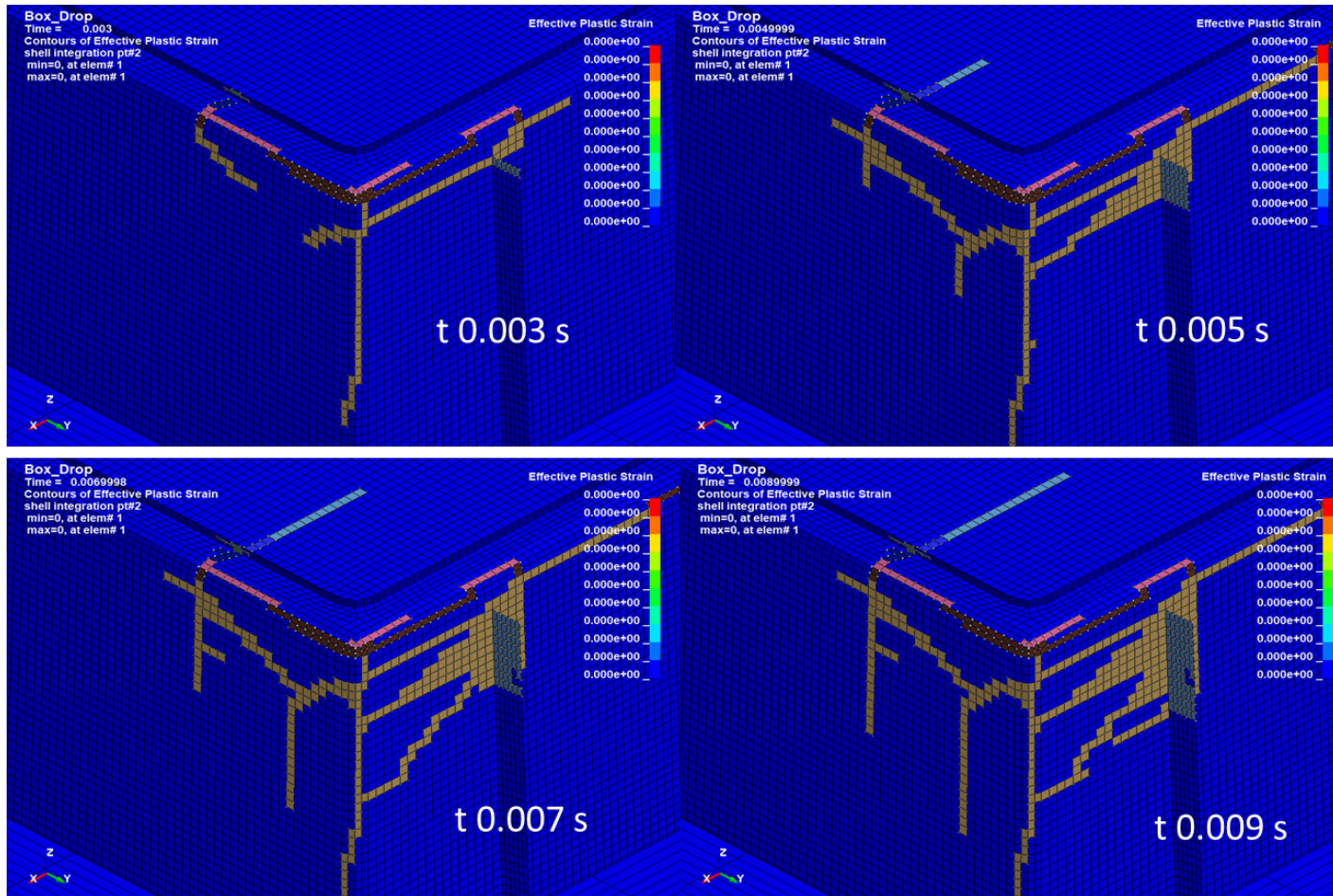
Four replications carried out under same testing conditions

Jaguar Land Rover test case: results

■ Simulation details

- *Digimat* 2017 (available and installed version) used with Ls-dyna
- Fiber orientation from JLR or varied (Folgar/Tucker, ARSC) from Moldflow
- Mesh size 2.5 mm (average)
- Element formulation 16
- Other parameters varied (Plasticity, mass scaling, FPGF and *Digimat* failure parameters, etc.)

Jaguar Land Rover test case: first simulation results

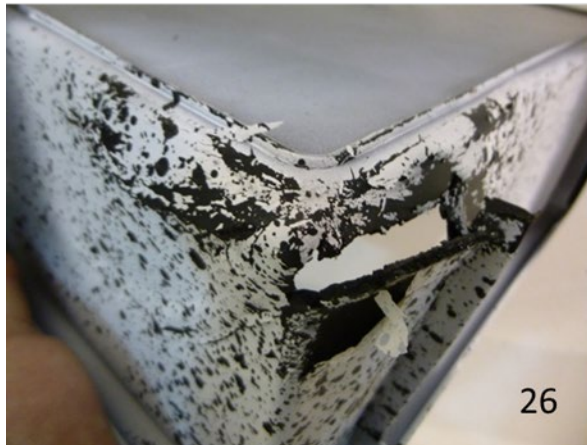


Plots of failed (deleted) elements

Source:
LyondellBasell

First results show unrealistic failure prediction, mainly related to fracture propagation

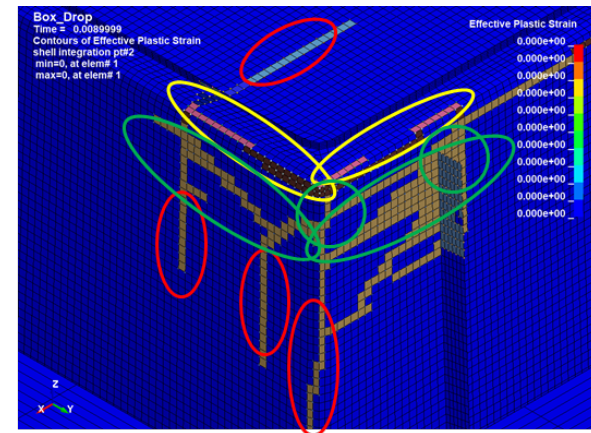
Jaguar Land Rover test case: first simulation results



Source: Jaguar Land Rover

Predicted fracture patterns

- Green circles: OK
- Red circles: BAD (propagation?)
- Yellow circles: BAD (mesh not accurate)

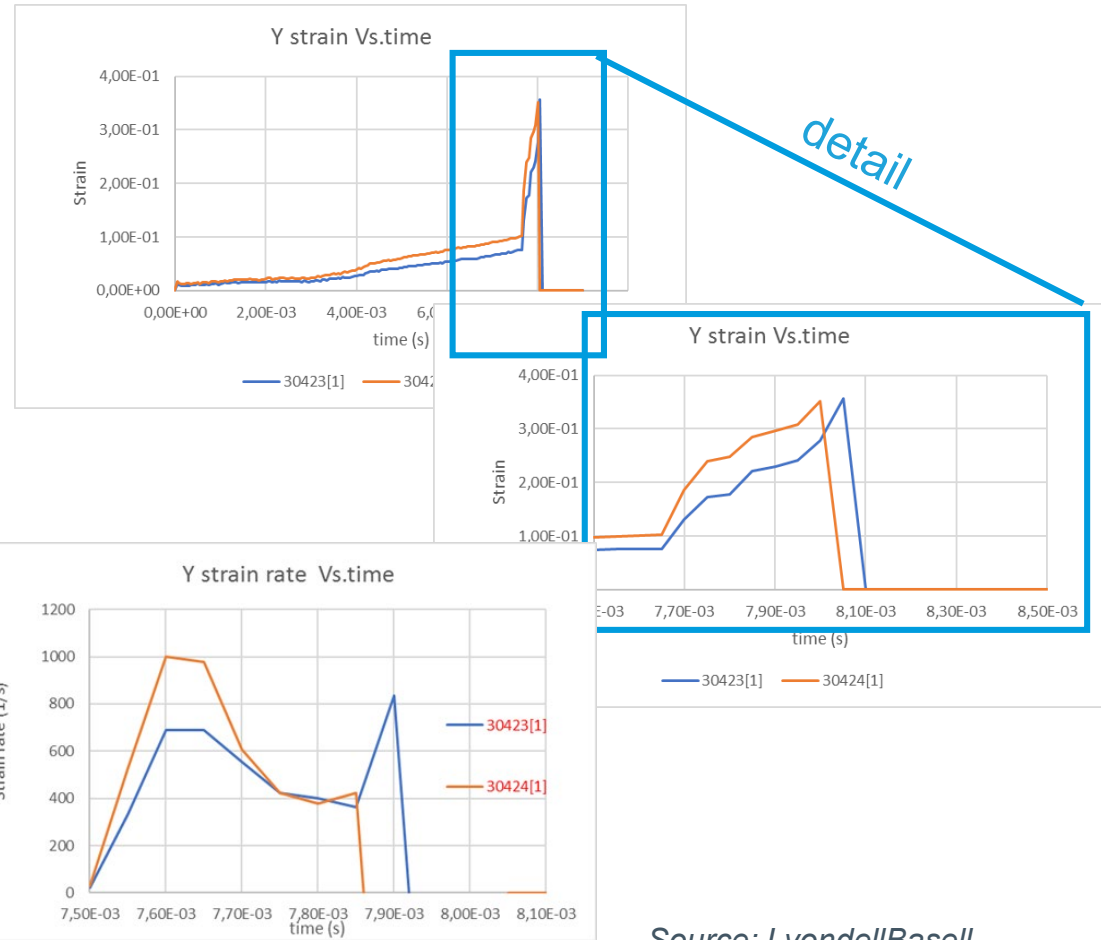
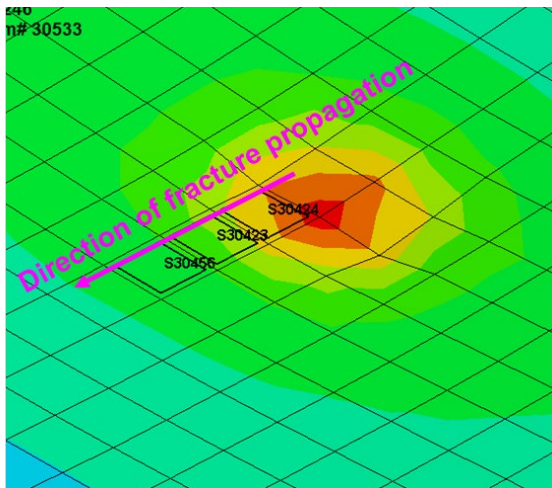


Source: LyondellBasell

First results show unrealistic failure prediction, mainly related to fracture propagation

Jaguar Land Rover test case: modifications

- Amendments and modifications: analysis and Interpretation of fracture propagation
 - Strain/ Strain rate peaks occur after the sudden elimination of an adjacent element due to the Failure Criterion functional reaching the threshold.



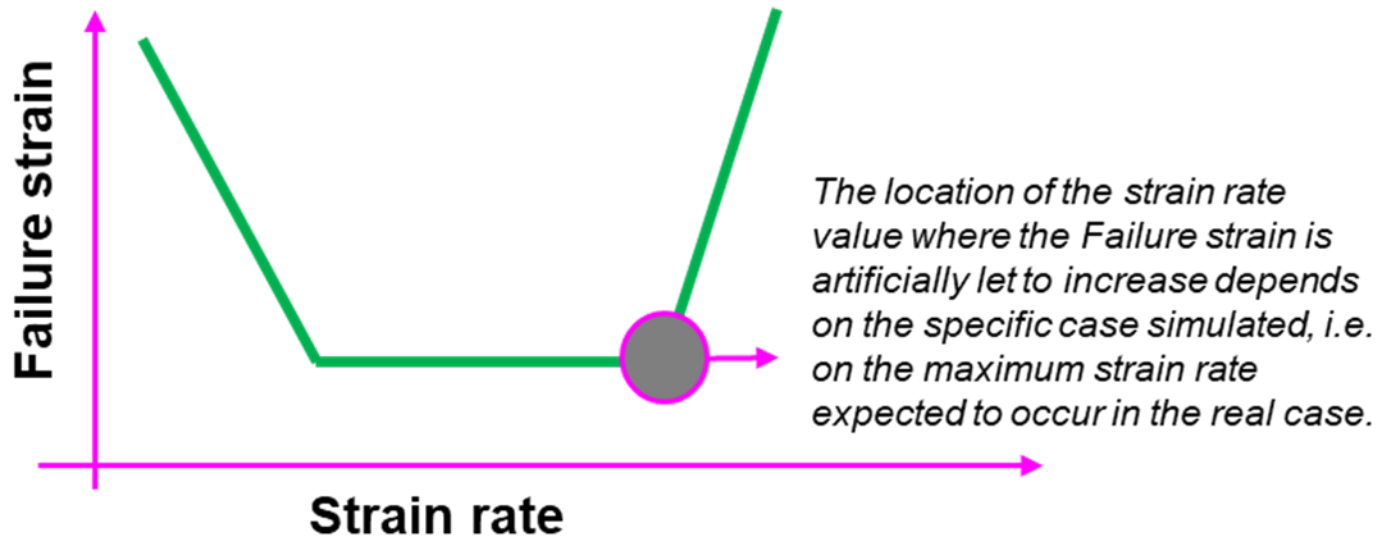
Source: LyondellBasell

Strain rate peaks occurring after element elimination mislead the failure criterion

Jaguar Land Rover test case: modifications

■ Amendments and modifications:

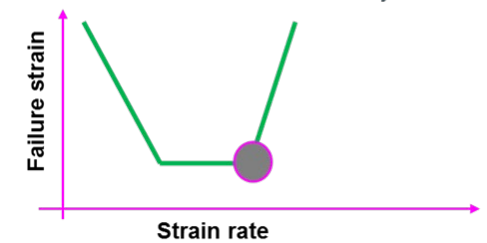
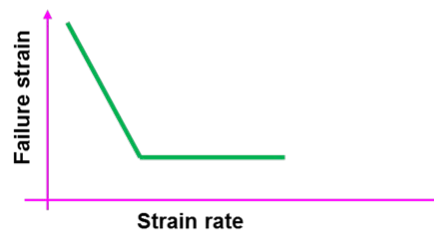
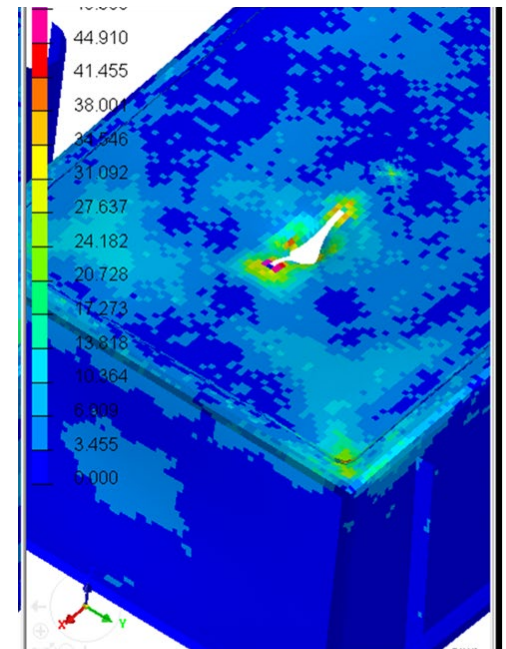
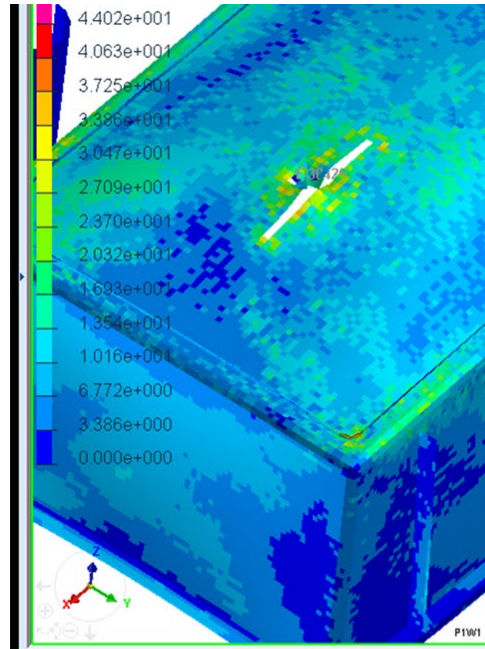
- “Washtube” shape for Failure strain vs. Strain rate to overcome failure criterion activation after contiguous element elimination
- Additionally: improvement in the mesh (location of the main rib)



Verification of the improvement on LyondellBasell test case

■ Results:

- “The modification seems to improve the prediction of the final fracture pattern on LYB Dart Test 1



Source: LyondellBasell

Source: LyondellBasell

Verification of the improvement on Jaguar Land Rover test case

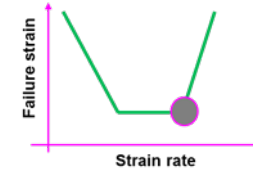
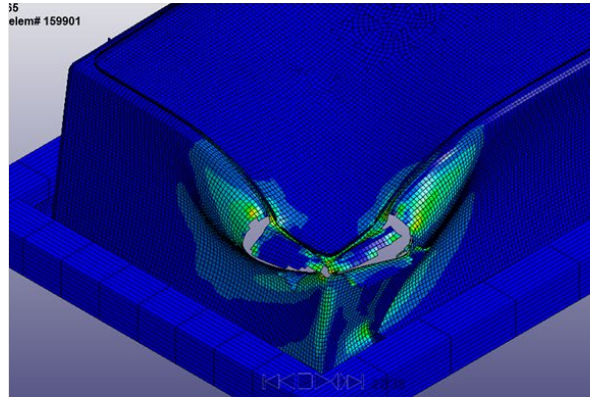
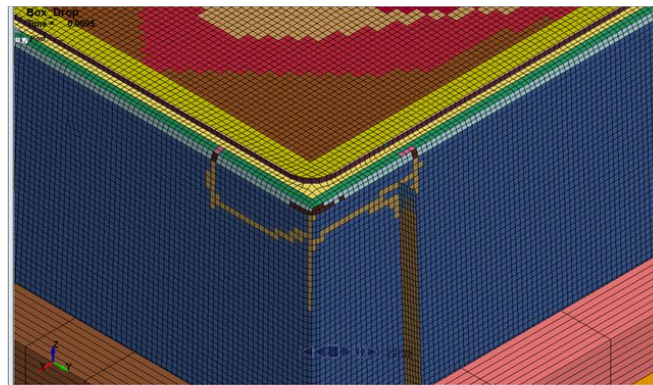


Image during the transient

Source:
LyondellBasell



Source: Jaguar Land Rover

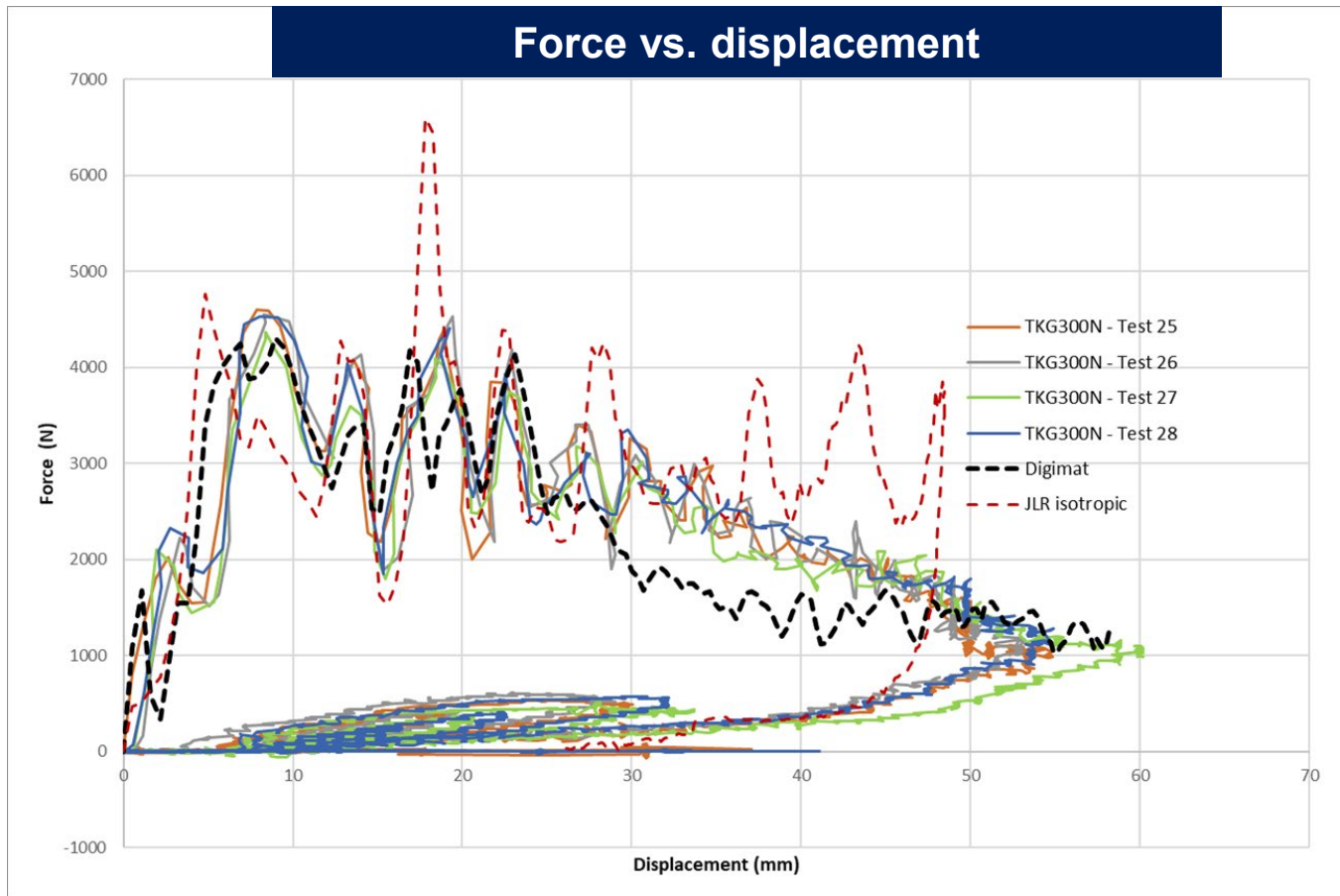


Predicted failed elements

Source:
LyondellBasell

Failure onset and fracture propagation are better predicted when proper dependence on strain rate is assumed for the failure criterion

Jaguar Land Rover test case: force vs. displacement



Source: LyondellBasell

Digimat predicts reasonable values in agreement with experimental curves

First conclusion

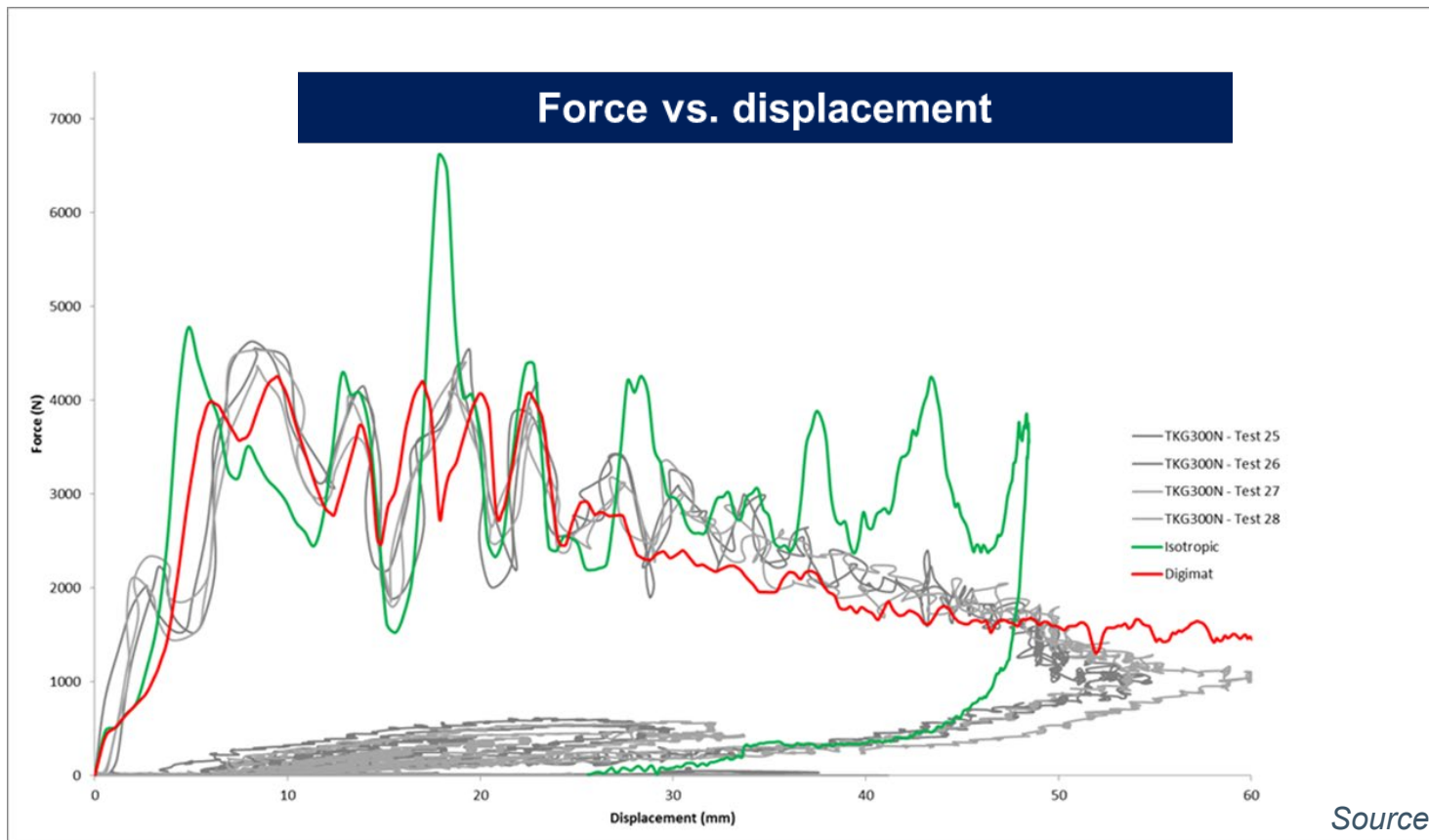
- The experimental data on two test cases were used to validate the material card for *Softell* grade
- The final predictions of force vs. Displacement curves in the two tests are definitely acceptable and aligned with the experimental evidence
- The Tsai-Wu failure criterion based on strain formulation performed well, provided that the strains were measured locally and a proper strain-rate dependence.
- This was conceived to block the activation of the criterion due to the strain rate peaks deriving from the deletion of failed elements
- Impact on parts made of *Softell* grades can be properly simulated with *Digimat*
- Can we do something better and in an easier way with *Digimat* 2018 and 2019 versions?

Impact on parts made of *Softell* grades can be properly simulated with *Digimat*

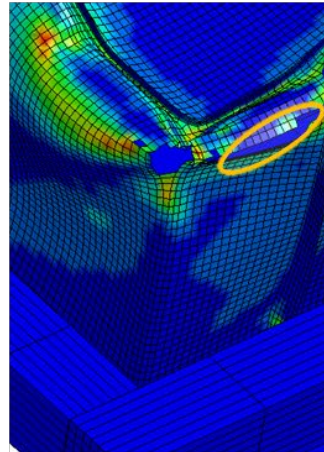
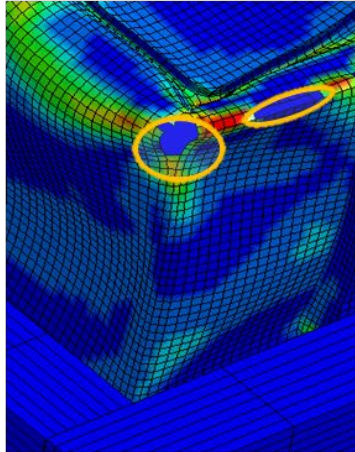
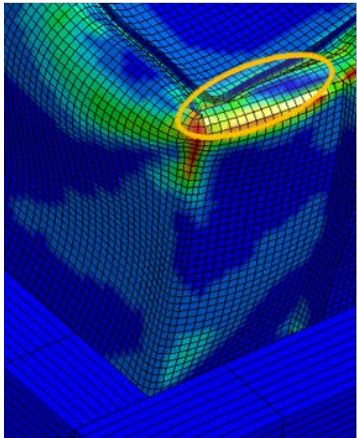
Can we do something better and in an easier way with *Digmat* 2018 and 2019 versions?

■ “*Ls-Dyna* 9.1.0 & *Digmat* 2018.1

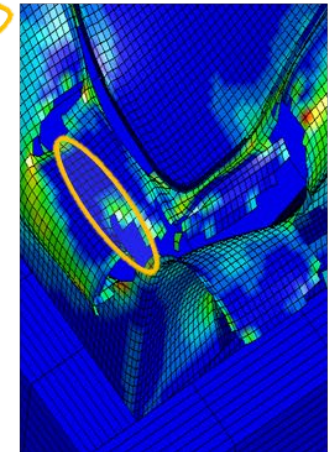
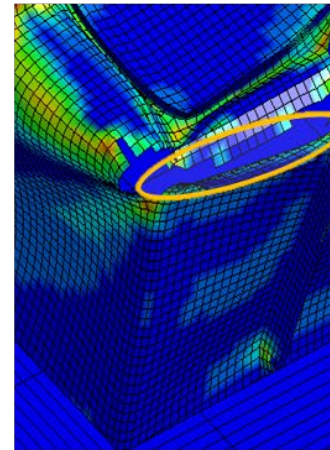
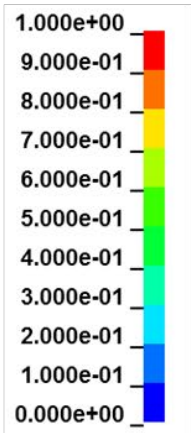
- The strain rate filtering parameter is a new to filter spurious oscillations of strain rate values during strain rate dependent FEA runs
- Applicable to failure models using a (V-)EVP material model



Can we do something better and in an easier way with *Digimat* 2018 and 2019 versions?



Source: Jaguar Land Rover



Source: e_Xstream

- Failure indicator is a *Digimat* output to detect the critical zone supposed to fail in the part
- When the value exceeds 1 this means that the element is deleted if no damage is included in the material law

Conclusion

Impact on parts made of *Softell* grades can be properly simulated with *Digimat*

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